



# Efficient reversible CO/CO<sub>2</sub> conversion in solid oxide cells with a phase-transformed fuel electrode

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**ABSTRACT** The reversible solid oxide cell (RSOC) is an attractive technology to mutually convert power and chemicals at elevated temperatures. However, its development has been hindered mainly due to the absence of a highly active and durable fuel electrode. Here, we report a phase-transformed CoFe-Sr<sub>3</sub>Fe<sub>1.25</sub>Mo<sub>0.75</sub>O<sub>7-δ</sub> (CoFe-SFM) fuel electrode consisting of CoFe nanoparticles and Ruddlesden-Popper-layered Sr<sub>3</sub>Fe<sub>1.25</sub>Mo<sub>0.75</sub>O<sub>7-δ</sub> (SFM) from a Sr<sub>2</sub>Fe<sub>7/6</sub>Mo<sub>0.5</sub>Co<sub>1/3</sub>O<sub>6-δ</sub> (SFMCo) perovskite oxide after annealing in hydrogen and apply it to reversible CO/CO<sub>2</sub> conversion in RSOC. The CoFe-SFM fuel electrode shows improved catalytic activity by accelerating oxygen diffusion and surface kinetics towards the CO/CO<sub>2</sub> conversion as demonstrated by the distribution of relaxation time (DRT) study and equivalent circuit model fitting analysis. Furthermore, an electrolyte-supported single cell is evaluated in the 2:1 CO-CO<sub>2</sub> atmosphere at 800°C, which shows a peak power density of 259 mW cm<sup>-2</sup> for CO oxidation and a current density of -0.453 A cm<sup>-2</sup> at 1.3 V for CO<sub>2</sub> reduction, which correspond to 3.079 and 3.155 mL min<sup>-1</sup> cm<sup>-2</sup> for the CO and CO<sub>2</sub> conversion rates, respectively. More importantly, the reversible conversion is successfully demonstrated over 20 cyclic electrolysis and fuel cell switching test modes at 1.3 and 0.6 V. This work provides a useful guideline for designing a fuel electrode through a surface/interface exsolution process for RSOC towards efficient CO-CO<sub>2</sub> reversible conversion.

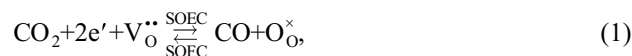
**Keywords:** reversible solid oxide cells, CO-CO<sub>2</sub> conversion, perovskite oxide, phase transformation, cyclic test

## INTRODUCTION

The demand for utilization and storage of renewable energy has been rapidly growing for decades as a result of the depletion of fossil fuels and fear of CO<sub>2</sub> emission. However, the nature of intermittency and variability makes only a small percentage of these energy systems available. To achieve a sustainable system, it is critical to develop energy conversion and storage technologies for clipping peak (shifting electricity from peak periods to off-peak periods), e.g., mountain water reservoirs, batteries, and reversible solid oxide cell (RSOC) systems [1,2].

Among all, RSOC has proven to be a highly effective technology for this purpose [3]. It can be reversibly operated by using CO<sub>2</sub> and H<sub>2</sub>O electrolysis to CO and H<sub>2</sub> (chemical energy carriers) in the solid oxide electrolysis cell (SOEC) mode and converting it back to generate electricity under the solid oxide fuel cell (SOFC) mode [4–6]. However, the development of RSOC remains a challenge due to many limitations. In particular, the electrochemical performance and durability are largely limited by the fuel electrode reaction instead of the oxygen electrode reaction, as expressed by Equations (1) and (2) using Kröger-Vink notations:

Fuel electrode



Oxygen electrode



where O<sub>O</sub><sup>×</sup> is an oxygen atom on the oxygen site with no

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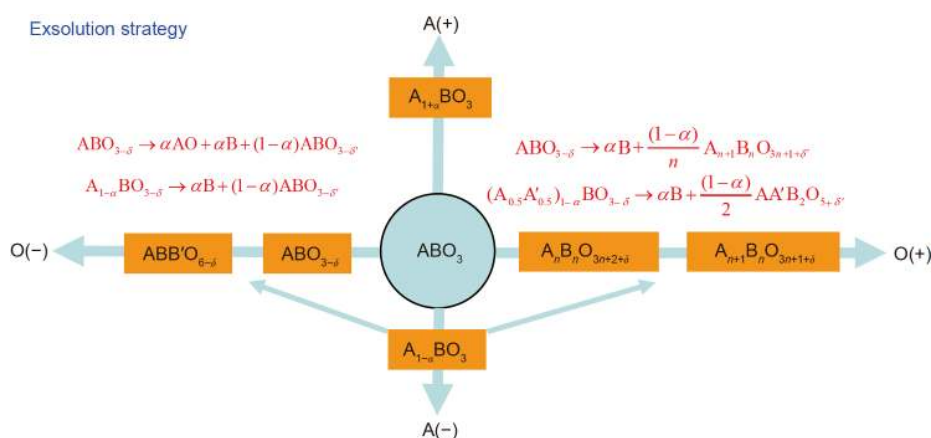
charge relative to the lattice, and  $V_{\text{O}}^{\bullet\bullet}$  is a vacancy on the oxygen site with two positive charges. The well-established Ni-YSZ ( $\text{Y}_2\text{O}_3$  stabilized  $\text{ZrO}_2$ ) fuel electrode is susceptible to degradation caused by coking and poisoning when it is used for  $\text{CO}$ - $\text{CO}_2$  conversion in RSOC, especially under the SOEC mode [7–10]. Ebbesen *et al.* [11] reported the rapid passivation of Ni-YSZ supported cells for  $\text{CO}_2$  reduction under the SOEC mode. It could not be fully recovered when operated under the SOFC mode to oxidize carbon. The addition of water steam for the  $\text{CO}_2$ - $\text{H}_2\text{O}$  coelectrolysis was proposed by Yan *et al.* [12], but this addition will increase the cost of the RSOC system during operation.

Recently, perovskite materials with mixed ionic and electronic conducting properties have been explored as alternative electrodes due to their excellent redox stability and high resistance to carbon deposition in the absence of water. For example,  $\text{La}(\text{Sr})\text{Cr}(\text{Mn})\text{O}_{3-\delta}$  [13,14],  $(\text{La})\text{SrTiO}_{3+\delta}$  [15], and several Fe-based materials [16] are most commonly studied. Unfortunately, the obtained electrochemical performances remain inferior compared with the Ni-YSZ composite [17]. Some studies have shown that the performance can be improved by introducing metal nanoparticles on the perovskite surface through various deposition techniques such as vapor deposition, infiltration, and exsolution [18–22].

Metal/alloy nanoparticles, which are *in situ* exsolved from perovskite oxide bulk to the surface, have gathered a considerable amount of interest because of their desired phase dispersion, strong aggregation and coking-resistance properties [23–28]. Typically, various reducible metal cations are incorporated into the B-site of the

perovskite lattice in the oxidizing atmosphere and subsequently exsolved as metallic nanoparticles on the perovskite surface under reducing conditions. Fig. 1 depicts a Cartesian plot of visual distinction for different chemical compositions and crystal structures upon the exsolution of B-site metals, where there are O-site and A-site nonstoichiometry as the  $x$ - and  $y$ -axes, respectively, and defect-free  $\text{ABO}_3$  as the origin. For an initially nonstoichiometric  $\text{ABO}_3$  (i.e.,  $A/B < 1$ ), the A-site deficiency can facilitate the diffusion of B-site cations for the exsolution process. For example, in the second quadrant, Neagu *et al.* [29] reported that Ni nanoparticles exsolved from  $\text{La}_{0.8}\text{Ce}_{0.1}\text{Ni}_{0.4}\text{Ti}_{0.6}\text{O}_{3+\delta}$  achieved large populations and exhibited superior catalytic activity and stability for the  $\text{CO}$  oxidation reaction. For an initial stoichiometric  $\text{ABO}_3$  (i.e.,  $A/B = 1$ ) perovskite, the exsolution of B-site cations can result in the formation of Ruddlesden-Popper (R-P) oxide phase *via* phase transformation. In the first quadrant, Liu *et al.* [30] reported that CoFe alloy nanoparticles were exsolved from  $\text{Pr}_{0.4}\text{Sr}_{0.6}\text{Co}_{0.2}\text{Fe}_{0.7}\text{Mo}_{0.1}\text{O}_{3-\delta}$  with the formation of  $(\text{Pr}_{0.4}\text{Sr}_{0.6})_3(\text{Fe}_{0.85}\text{Mo}_{0.15})_2\text{O}_7$  with the R-P layered structure, which enhanced the  $\text{CO}_2$  electrolysis performance in SOEC. Similar results were also reported for SOFC using hydrogen or hydrocarbon fuels [31,32], which highlighted excellent resistance to carbon deposition and sulfur poisoning. Hence, this exsolution strategy will highly likely play a significant role in RSOC for the  $\text{CO}/\text{CO}_2$  conversion, which has not been reported in the literature to the best of our knowledge.

Remarkably, Fe-based perovskites demonstrate the desired conductivity, high redox stability, and acceptable electrocatalytic activity. Inspired by these insights, we designed an Fe-rich perovskite  $\text{Sr}_2\text{Fe}_{7/6}\text{Mo}_{0.5}\text{Co}_{1/3}\text{O}_{6-\delta}$



**Figure 1** Cartesian plot that anticipates the key role of perovskite nonstoichiometry for the *in situ* exsolution process, where the  $x$ - and  $y$ -axes correspond to oxygen-site and A-site nonstoichiometry, respectively. Deficiency and excess are indicated by (-) and (+), respectively.

(SFMCo), which is phase-transformed into CoFe alloy and R-P layer-structured  $\text{Sr}_3\text{Fe}_{1.25}\text{Mo}_{0.75}\text{O}_{7-\delta}$  (SFM) composite after being annealed in hydrogen. In this work, this novel material is used as the fuel electrode to facilitate the CO/CO<sub>2</sub> conversion kinetics and enhance the resistance against carbon deposition in RSOC. Furthermore, we evaluated the electrochemical performance of RSOC with this fuel electrode and demonstrated the reversible operation under cyclic SOFC and SOEC modes.

## EXPERIMENTAL SECTION

### Powder preparation

SFMCo powders were synthesized using a conventional citric-glycine combustion method. Stoichiometric amounts of chemicals  $\text{Sr}(\text{NO}_3)_2$ ,  $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ ,  $(\text{NH}_4)_6\text{Mo}_7\text{O}_{24} \cdot 4\text{H}_2\text{O}$  and  $\text{Co}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  (all from Sinopharm Chemical Reagent Co., Ltd) were dissolved in deionized water using citric acid and glycine as complexing agents. By evaporating *via* a stove plate, a dark purple gel was obtained. Then, the gel was calcined at 1000°C for 5 h to obtain SFMCo powders. The reference sample  $\text{Sr}_2\text{Fe}_{1.5}\text{Mo}_{0.5}\text{O}_{6-\delta}$  (P-SFM) was synthesized using the same method. After annealing in a quartz tube under flowing hydrogen at 800°C for 2 h, SFMCo samples were transformed into CoFe alloy and R-P layer-structured  $\text{Sr}_3\text{Fe}_{1.25}\text{Mo}_{0.75}\text{O}_{7-\delta}$  (CoFe-SFM for short).  $\text{Sm}_{0.2}\text{Ce}_{1.8}\text{O}_{2-\delta}$  (SDC) powders were synthesized by the coprecipitation method [33].  $(\text{La}_{0.85}\text{Sr}_{0.15})_{0.9}\text{MnO}_{3-\delta}$  (LSM) powders were synthesized by the glycine combustion [34].  $(\text{Y}_2\text{O}_3)_{0.08}(\text{ZrO}_2)_{0.92}$  (YSZ, Fuel Cell Materials, USA) powders were used without further treatment as the electrolyte.

### Fabrication of the symmetrical cells and single cells

The symmetrical cell was composed of one YSZ electrolyte substrate, two electrode layers, and two SDC buffer layers between the electrolyte and electrode. Dense YSZ electrolyte substrates (~200 μm in thickness) were prepared by dry pressing powders under ~400 MPa and subsequent sintering at 1450°C for 5 h in air. An SDC layer was screen-printed onto both sides of the YSZ surface and sintered at 1200°C for 3 h. In addition, the SFMCo layer was screen-printed onto the SDC surface and sintered at 1000°C for 2 h. For the single cell with the SFMCo/SDC//YSZ//LSM-SDC configuration, the LSM-SDC (6:4 in the mass ratio) layer was screen-printed onto the other surface of YSZ and subsequently calcined at 1200°C for 2 h. Ag (current collector) paste was deposited onto the SFMCo and LSM-SDC surfaces and heat treated

at 500°C for 1 h.

### Characterization methods

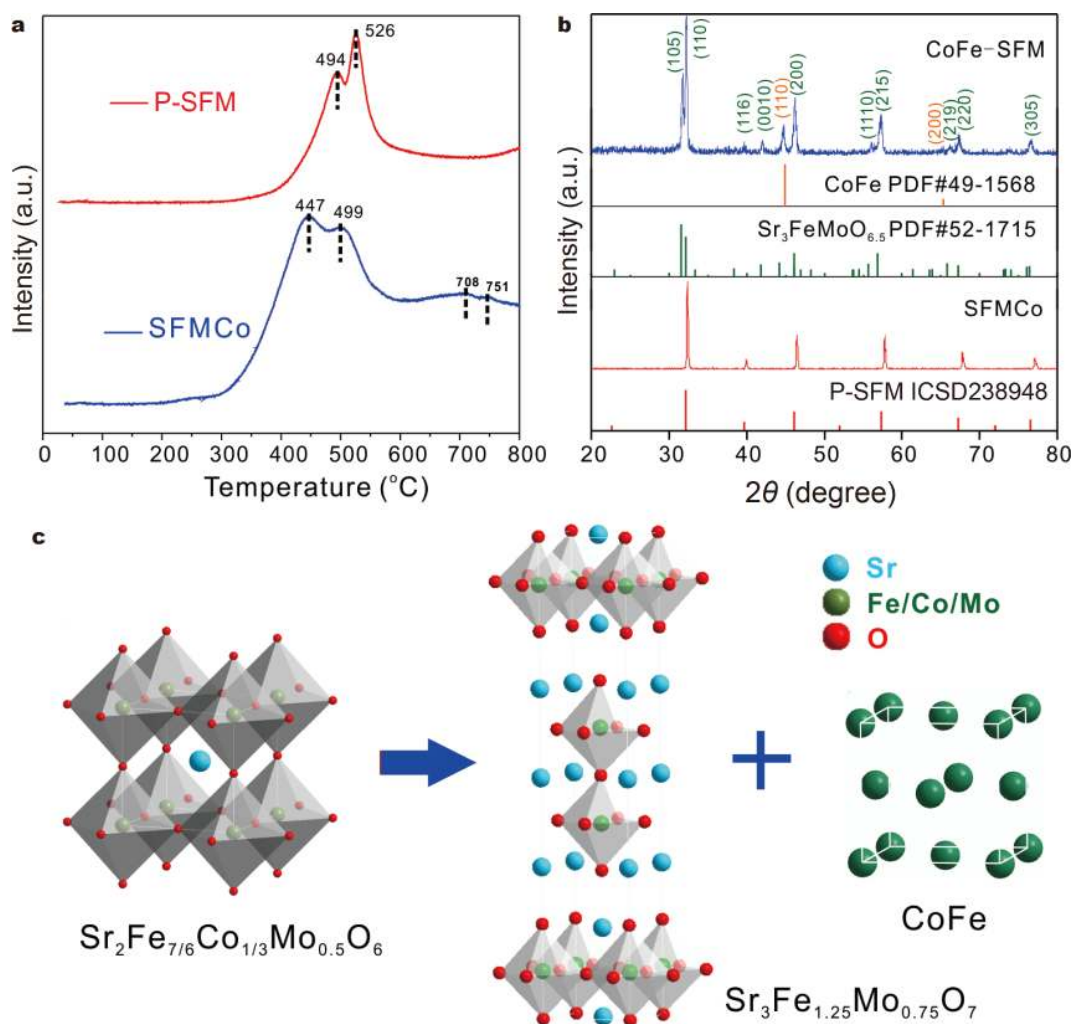
X-ray diffraction (XRD) analyses were conducted using a Rigaku TTR-III diffractometer with a Cu Kα radiation source. High-resolution transmission electron microscopy (HRTEM) and the corresponding energy dispersive X-ray (EDX) mapping analyses were performed on a JEOL JEM-F200 TEM/STEM. X-ray photoelectron spectroscopy (XPS, ESCALAB 250) was used to investigate the chemical states of the elements. The microstructures of the cells and their electrodes were analyzed using field emission scanning electron microscopy (FE-SEM, JEOL JSM7000F). H<sub>2</sub> temperature-programmed reduction (H<sub>2</sub>-TPR) experiments were performed using TPDRO 1100 from 40 to 800°C. Symmetrical cells were investigated at 700–850°C under 2:1 CO-CO<sub>2</sub> ( $P_{\text{O}_2} = 9.49 \times 10^{-20}$  atm at 800°C) atmosphere.

### Electrochemical performance measurement

The electrochemical impedance spectroscopy (EIS) was conducted in the frequency range of 0.01–1 MHz (Solarton 1260) under open-circuit voltage (OCV) conditions. Single cells were sealed on an alumina tube using conductive resins. Before the test, the fuel electrode was annealed in hydrogen at 800°C for 2 h, and the LSM-SDC oxygen electrode was exposed in ambient air. Afterward, the feeding gas was switched to 2:1 CO-CO<sub>2</sub> at a flow rate of 50 mL min<sup>-1</sup>. Polarization characteristics (*I*-*V* curves) and EIS of single cells were measured through a two-electrode configuration using Solarton 1287 & 1260. The distribution of relaxation time (DRT) method was applied to deconvolute EIS using DRT tools from Francesco's group [35,36], where the regularization parameter was set to 10<sup>-3</sup>.

## RESULTS AND DISCUSSION

The CoFe alloy exsolution process was accompanied by the phase transformation of the SFMCo perovskite parent. First, the corresponding reduction-exsolution temperature was analyzed by H<sub>2</sub>-TPR, as shown in Fig. 2a. For reference sample P-SFM [37], the reduction of Fe<sup>*n*+</sup> (*n* = 3 and 4) likely occurs in two main steps, i.e., the two peaks at 494°C and 526°C, which correspond to the reduction of Fe<sup>4+</sup> → Fe<sup>3+</sup> and Fe<sup>3+</sup> → Fe<sup>2+</sup>. When Co is doped into P-SFM to form SFMCo, the first reduction peak is reduced to 447°C, and the second reduction peak is reduced to 499°C. Two additional overlapped peaks appear at 708 and 751°C, which should correspond to the reduction of Co<sup>*n*+</sup> (*n* = 2, 3 and 4) into metallic Co<sup>0</sup> and Fe<sup>2+</sup>

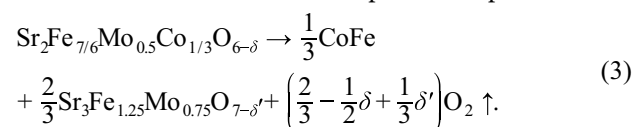


**Figure 2** (a)  $\text{H}_2$ -TPR profiles of P-SFM [37] and CoFe-SFM samples; (b) XRD patterns of SFMCo and CoFe-SFM powders; (c) illustration model for the structural transformation of SFMCo (cubic) to SFM (tetragonal) and CoFe alloy (cubic).

into  $\text{Fe}^0$ , respectively. This process depicts the temperature window of exsolution and phase transformation from SFMCo into CoFe alloy and SFM. To remarkably facilitate this transformation process, the reduction temperature was set to  $800^\circ\text{C}$  and maintained for 2 h.

Fig. 2b shows the XRD patterns of the as-prepared SFMCo and reduced SFMCo powders. The SFMCo sample exhibits a cubic perovskite with the  $Pm\bar{3}m$  space group like the isostructural P-SFM (ICSD-238948) [38], which implies that Co has been well doped into SFM perovskite without causing any structural change or formation of the secondary phase. After a reduction in  $\text{H}_2$  at  $800^\circ\text{C}$  for 2 h, the pure perovskite phase is transformed into two different phases: an R-P phase and an alloy phase. The R-P phase can be well indexed with tetragonal  $\text{Sr}_3\text{FeMoO}_{6.5}$  (PDF#52-1715), while the alloy phase cor-

responds to cubic CoFe alloy (PDF#49-1568). The above information reveals the feasibility of this strategy. Therefore, the phase transformation of SFMCo can be mathematically expressed as Equation (3), since all Co were exsolved from the SFMCo perovskite parent.



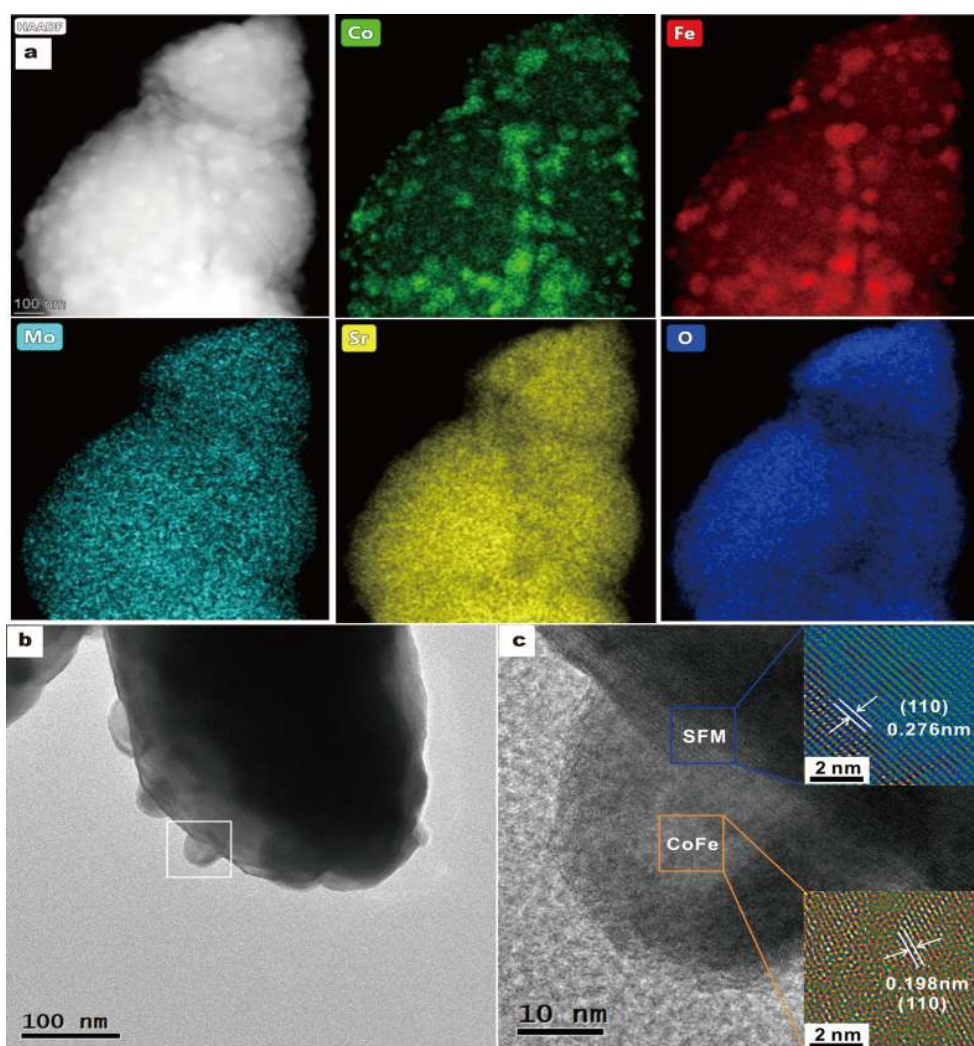
Furthermore, Fig. 2c depicts the illustration model for the structural transformation of cubic SFMCo to tetragonal SFM and cubic CoFe alloy. As observed, SFM exhibits a type of R-P layered structure ( $A_nB_nO_{3n+1}$ ,  $n = 2$  in our case), where the  $[\text{Sr}_2\text{Fe}_{1.25}\text{Mo}_{0.75}\text{O}_{6-\delta}]$  perovskite layer and  $[\text{Sr}-\text{O}]$  rock-salt layer are alternately arranged along the  $c$ -axis. As suggested in other studies [32,39,40], these

materials show excellent thermal and structural stabilities.

The chemical compositions and microstructure were further investigated. Fig. 3a shows the distribution of elements for the CoFe-SFM sample under the high-angle annular dark field (HAADF) mode. Sr, Fe, Mo, Co, and O were found in CoFe-SFM. Unlike the uniform distribution of Sr, Mo and O elements, partial Fe (bright red) and almost all Co (bright green) have been exsolved from the perovskite oxide parent. Because they are at the same location, exsolved Co and Fe exist in the form of alloy (solid solution), which is consistent with the XRD analysis. As reported by Gao *et al.* [41], the exsolution process consists of four steps: cation diffusion, reduction, nucleation, and particle growth. In the case of SFMCo, first, Co and Fe cations diffuse from the bulk to the

surface or near the surface; then, they were reduced to metallic  $\text{Co}^0$  and  $\text{Fe}^0$ . Subsequently, the initially formed  $\text{Co}^0$  and  $\text{Fe}^0$  nuclei are combined into fine alloy nanoparticles through the local near-surface migration.

The detailed TEM image is shown in Fig. 3b. The dispersed CoFe nanoparticles in the range of 20–50 nm are socketed on the SFM substrate by being submerged near the surface. The resulting interface (a close curve) indicates the strong interaction between nanoparticles and perovskite oxide parents because the CoFe lattice is undeniably epitaxially grown from the perovskite oxide lattice [42]. Fig. 3c presents an enlarged view of the white rectangle in Fig. 3b to identify the lattice fringe orientation and interplanar spacing. The interplanar spacing of nanoparticles (orange rectangle) is 0.198 nm, which cor-



**Figure 3** (a) HAADF image of CoFe-SFM powders and corresponding elemental mapping; (b) TEM image of a typical CoFe-SFM sample; (c) enlarged view of the white rectangle of b (Insets are HRTEM images of CoFe nanoparticles and SFM, respectively).

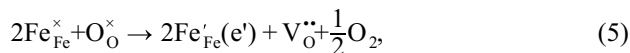
responds to the (110) planes of the CoFe alloy phase. The interplanar spacing of parent oxide (blue rectangle) is 0.276 nm, which is similar to the (110) planes of the SFM crystalline phase.

Oxygen vacancies are very crucial to electrode materials, which are required for oxygen ion transport from the electrode to the electrolyte. In addition, surface oxygen vacancies act as host sites for the adsorption and activation of CO/CO<sub>2</sub> molecules [43]. In this regard, XPS measurement was conducted to investigate the chemical state of oxygen species; and the results are shown in Fig. S1. Given Gaussian fitting, three binding energy components are observed in the CoFe-SFM sample (Fig. S1a), which are deconvoluted into a low-energy peak, a middle-energy peak, and a high-energy peak centered at 529.51, 531.17, and 532.63 eV, respectively. The low-energy peak comes from lattice oxygen ions (O<sub>L</sub>, 1.95%) on the intrinsic sites. The middle-energy peak is attributed to undercoordinated oxygen-containing species (O<sub>S</sub>, 74.93%), which is positively related to the oxygen vacancy concentrations [44]. Since SFM has a layer structure, which consists of a perovskite layer and a rock salt layer, the oxygen vacancies and interstitial oxygen (O<sub>i</sub><sup>••</sup>, 23.12%) ions can coexist in the SFM lattice, which are accommodated on octahedral sites and tetrahedral interstitial sites, respectively [45,46]. Based on this information, the high-energy peak is assigned to interstitial oxygen ions (O<sub>i</sub><sup>••</sup>) [47,48], which can be interpreted as the formation of an anion Frenkel-type defect on the oxygen sublattice as follows:



where O<sub>i</sub><sup>••</sup> is an oxygen ion on an interstitial site with two negative charges. The [Sr–O] rock-salt layer contributes to O<sub>i</sub><sup>••</sup> transport along the *a-b* plane by an interstitial (push-pull) mechanism between interstitial and apical oxygen sites from the Fe(Mo)O<sub>6</sub> octahedra, whereas the [Sr<sub>2</sub>Fe<sub>1.25</sub>Mo<sub>0.75</sub>O<sub>6-δ</sub>] perovskite layer with oxygen vacancies is responsible for the transport of lattice oxygen ions *via* 3-dimensional vacancies by the hopping mechanism [45]. The coexistence of these two types of defects is very favorable for the solid-gas oxygen exchange reaction and bulk oxygen ion diffusion in typical solid oxide cell conditions [49,50]. Unlike the CoFe-SFM sample, two binding energy components are only observed in the SFMCo sample (Fig. S1b), while O<sub>L</sub> and O<sub>S</sub> account for 53.23% and 46.77%, respectively. It should be noted that SFM-based material systems show an n-type conducting behavior in a reducing atmosphere [43]. During the phase-transformation process, the partial Fe

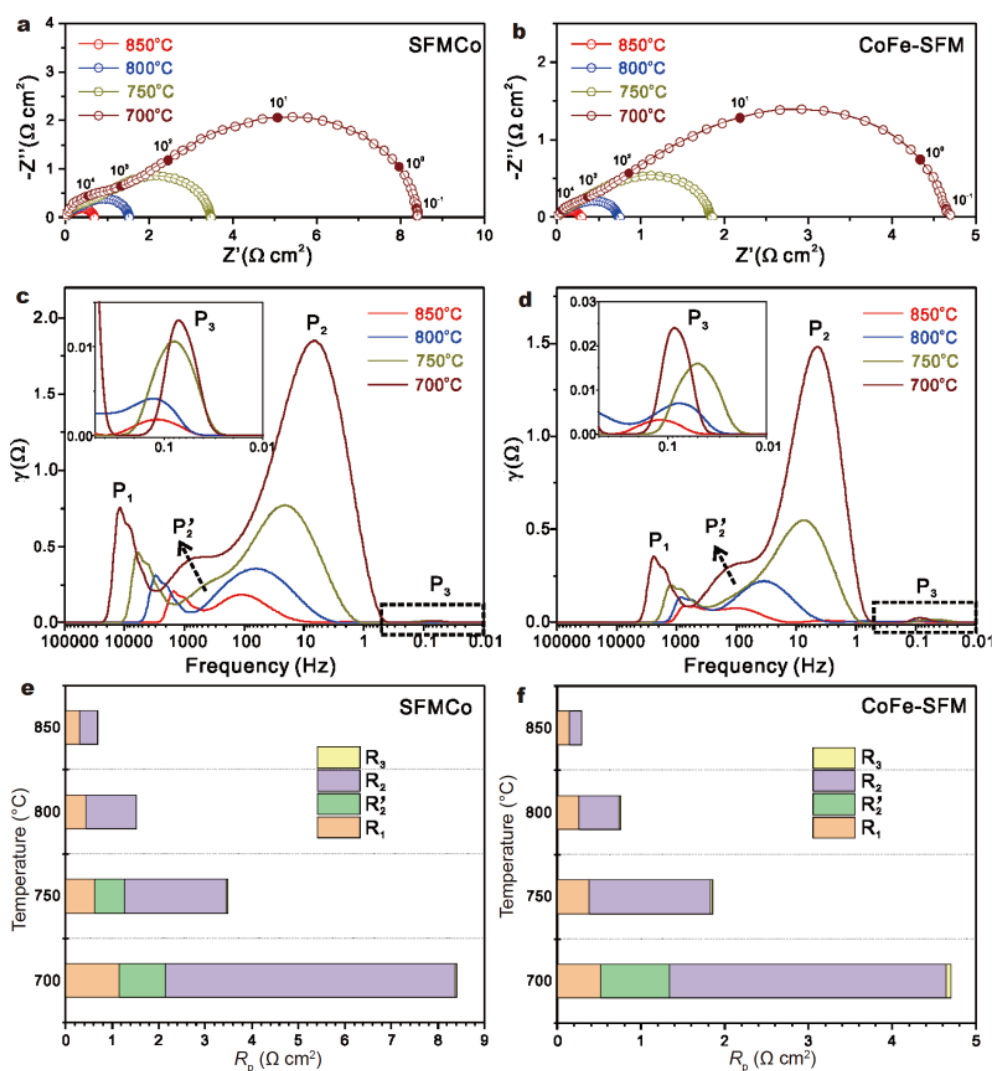
cations are reduced to lower oxidation states when lattice oxygen is removed, which increases the concentrations of both oxygen vacancies and electrons as follows:



where Fe<sub>Fe</sub><sup>×</sup> is an Fe<sup>3+</sup> cation on the Fe site with no charge relative to the lattice, and Fe'<sub>Fe</sub> is an Fe<sup>2+</sup> cation on the Fe site with a negative charge relative to the lattice. These positive effects are expected to improve the catalytic activity of the fuel electrode towards the CO/CO<sub>2</sub> conversion.

The electrochemical catalytic activities of the fuel electrode for the CO-CO<sub>2</sub> conversion reaction were investigated by EIS plots using YSZ-supported symmetrical cells (SFMCo/SDC/YSZ/SDC/SFMCo and CoFe-SFM/SDC/YSZ/SDC/CoFe-SFM) in a 2:1 CO-CO<sub>2</sub> atmosphere. SDC as the buffer layer was also significantly reduced, which results in a behavioral change of the pure ionic conductor to a mixed ionic-electronic conductor. Fig. 4a, b display the Nyquist plots of EIS for SFMCo and CoFe-SFM fuel electrodes at 700–850°C under OCV conditions. To intuitively compare the electrode polarization resistance (R<sub>p</sub>), all first intercepts with Z'-axis were simplified to zero by subtracting the real ohmic resistance [51]. The difference between the two Z'-axis intercepts at the high frequency and low frequency of each impedance plot represents the R<sub>p</sub> value. The R<sub>p</sub> value reflects the catalytic activity towards the CO/CO<sub>2</sub> conversion reaction; a lower R<sub>p</sub> value indicates a higher activity and *vice versa*. In Fig. 4a, the R<sub>p</sub> values of the SFMCo fuel electrode are determined to be 0.687, 1.523, 3.475 and 8.402 Ω cm<sup>2</sup> at 850, 800, 750 and 700°C, respectively. In contrast, the corresponding R<sub>p</sub> values are reduced to 0.292, 0.750, 1.855, and 4.699 Ω cm<sup>2</sup> for CoFe-SFM, which indicates better electrocatalytic activity of the CoFe-SFM fuel electrode (Fig. 3b) under the same condition. For example, at 800°C, the fuel electrode performance is promoted by 51% after reduction and exsolution, which implies that the CO/CO<sub>2</sub> conversion kinetics is greatly improved in practical single cells.

The Nyquist plots in EIS can be considered a “superposition” of a series of electrode processes that occur on the electrode. It is very challenging to identify the overlapped arcs using conventional Bode plots with lower resolution [52,53]. To determine the improvement mechanism of the CO/CO<sub>2</sub> conversion activity on the phase-transformed CoFe-SFM fuel electrode, a DRT method was utilized by deconvoluting EIS data [35]. Different electrode processes can be effectively separated with a



**Figure 4** Electrochemical performance comparison of (a, c, e) SFMCo and (b, d, f) CoFe-SFM fuel electrodes in a 2:1 CO-CO<sub>2</sub> atmosphere at 700–850°C. (a, b) Nyquist plots, (c, d) DRT profiles, and (e, f) fitted resistance values of the identified peaks.

high resolution based on the respective characteristic frequencies. As shown in Fig. 4c, the response for the SFMCo fuel electrode is mainly contributed by two peaks ( $P_1$  and  $P_2$ ) at 800 and 850°C, whereas the third peak  $P_3$  shows a negligible effect. The CoFe-SFM fuel electrode exhibits similar results at 750–850°C (Fig. 4d). However, a new peak  $P'_2$  appears between  $P_1$  and  $P_2$  at 750 and 700°C for the SFMCo fuel electrode, while it appears at 700°C for the CoFe-SFM fuel electrode. Based on the predefined evaluation of EIS plots by the DRT curves, equivalent circuit models (ECMs) were determined, e.g., three series (R//CPE) circuits at 750–850°C and four series (R//CPE) circuits at 700°C for the CoFe-SFM fuel electrode. Each ( $R_i$ //CPE<sub>*i*</sub>) circuit model represents a possible electrode

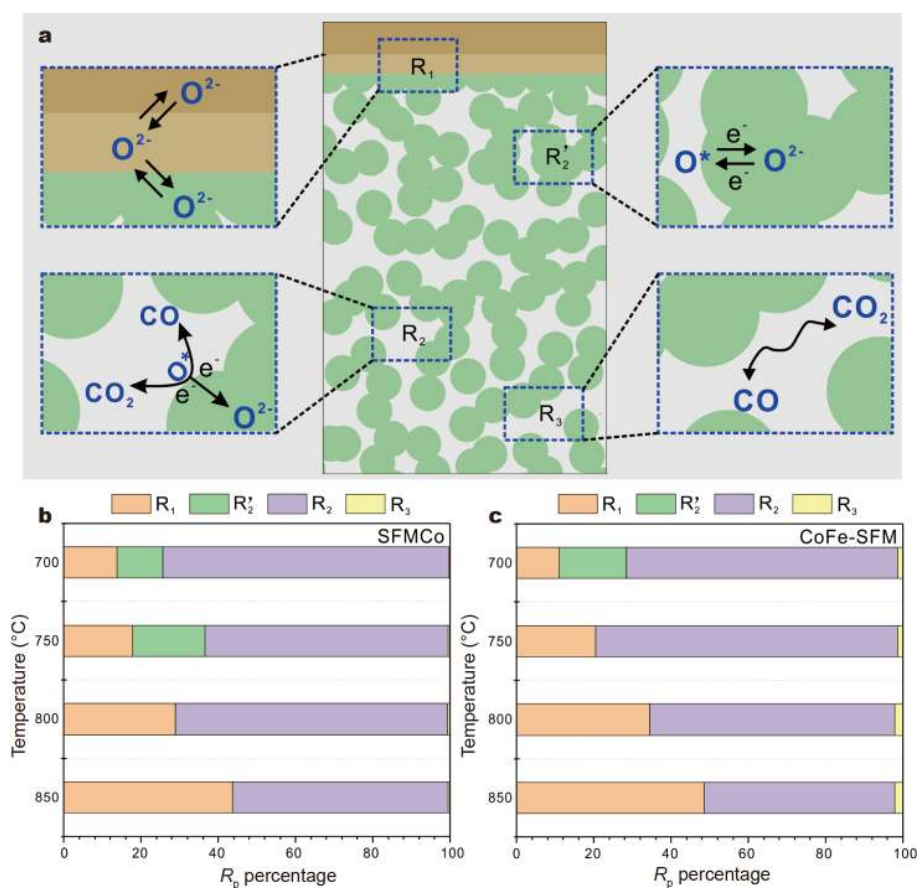
substep, while R and CPE are the resistor and constant-phase element, respectively.

In Fig. 4a, b, the Nyquist plots were fitted using the complex nonlinear least-square method in Z-view software to obtain a series of resistance values, which correspond to the identified peaks in Fig. 4c, d, as summarized in Table S1 and shown in Fig. 4e, f. At 800°C,  $R_1$  and  $R_2$  are largely reduced from 0.440 and 1.074  $\Omega\text{ cm}^2$  for the SFMCo fuel electrode (Fig. 4e) to 0.258 and 0.476  $\Omega\text{ cm}^2$  for the CoFe-SFM fuel electrode (Fig. 4f). However, the negligible  $R_3$  increases from 0.009 to 0.016  $\Omega\text{ cm}^2$ . At 700°C, the first two peaks ( $R_1$  and  $R_2$ ) are also largely reduced from 1.156 to 0.520  $\Omega\text{ cm}^2$  for  $R_1$  and from 6.221 to 3.303  $\Omega\text{ cm}^2$  for  $R_2$ . For the additional  $R'_2$ , the value is

slightly reduced from 0.995 to 0.816  $\Omega \text{ cm}^2$ . In the meanwhile,  $R_3$  increases from 0.03 to 0.06  $\Omega \text{ cm}^2$  at 700°C. Based on these impartial data, the high-resolution DRT method provides further insight into the resistance improvement on the phase-transformed CoFe-SFM fuel electrode.

In Fig. 4c, d, both  $P_1$  and  $P_2$  are significantly decreased and thermally activated. As suggested by the Adler-Lane-Steele model [54,55] and our previous work [37,43],  $P_1$  at high frequency is correlated with the oxygen transport across the electrolyte (YSZ)-buffer layer (SDC), interface-fuel electrode interface (CoFe-SFM) and solid-state diffusion through the fuel electrode bulk. The improvement of  $P_1$  may imply that SDC and SFM were deeply reduced during annealing in hydrogen.  $P_2$  at medium frequency is assigned to the polarization loss of the CO/CO<sub>2</sub> conversion reaction on the fuel electrode surface, which consists of the electron transfer, surface oxygen exchange, and CO<sub>2</sub> dissociation/CO binding to O<sup>\*</sup> at the gas-electrode interface. The significant decrease of  $P_2$  is entirely due to

the phase-transformed fuel electrode, which consists of CoFe alloy with excellent activity and SFM with abundant oxygen vacancies and interstitial oxygen ions (Fig. S1a). The reaction active sites were expanded from the SFM surface to the gas-CoFe-SFM interface. Since the virtually negligible  $P_3$  is located at low frequency ( $\leq 0.1$  Hz), it can be undoubtedly ascribed to gas diffusion. The larger values for CoFe-SFM than the SFMCo fuel electrode can be explained by the slight difference in the porosity of these two electrodes. Interestingly,  $P'_2$  appears at temperatures below 750°C for the SFMCo fuel electrode but 800°C for the CoFe-SFM fuel electrode. As a shoulder peak, it appears to be separated from  $P_2$ . The effective capacitance of  $P'_2$  for the CoFe-SFM fuel electrode is calculated to be approximately  $9 \times 10^{-4}$  F, which is associated with the charge transfer ( $10^{-4}$ – $10^{-5}$  F) for the oxygen exchange process [56]. This value is reasonable because electron-rich CoFe alloy is exsolved on the SFM surface, which increases the local electronic conductivity [51]. Through the above analysis and attribution, these four different



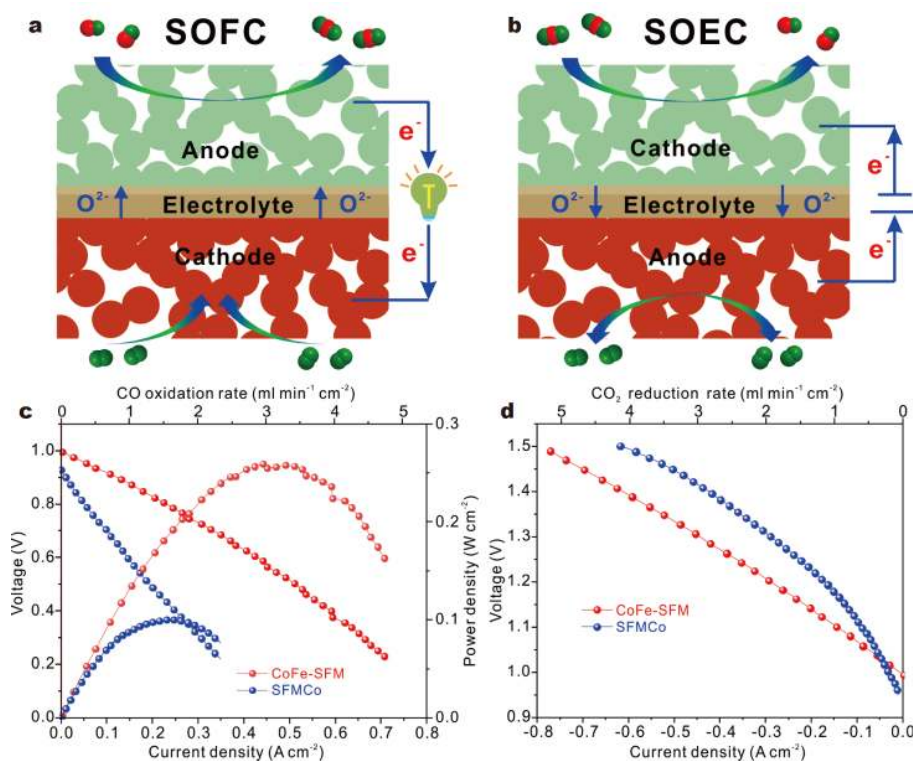
**Figure 5** (a) Schematic diagram of four polarization processes in the fuel electrode towards the CO<sub>2</sub>/CO conversion. (b, c) Calculated proportions of four polarization resistances in the SFMCo and CoFe-SFM fuel electrodes.

electrode substeps towards the CO/CO<sub>2</sub> conversion reaction are depicted in Fig. 5a. Therefore, it is evident from our comparative study that the phase-transformed fuel electrode can accelerate both surface/interface conversion kinetics and bulk oxygen transport processes except for gas diffusion.

To understand how the contribution of each substep evolves relative to one another with decreasing temperature, the percentages of four resistances to the total resistance were calculated, as summarized in Table S2 and shown in Fig. 5b, c. For the SFMCo fuel electrode (Fig. 5b),  $R_2$  accounts for the largest proportion at all operating temperatures (55.90% at 850°C, 70.52% at 800°C, 62.88% at 750°C and 74.04% at 700°C, Table S2), which indicates that the CO/CO<sub>2</sub> conversion reaction remains limited by the surface kinetics. For the CoFe-SFM fuel electrode in Fig. 5c, similar results are observed at 700–800°C (63.47% at 800°C, 78.28% at 750°C and 70.30% at 700°C as shown in Table S2). At 850°C,  $R_1$  (48.63%) and  $R_2$  (49.32%) are almost equal, which indicates that the CO/CO<sub>2</sub> conversion reaction is colimited by the oxygen transport/diffusion and surface kinetics for the CoFe-SFM fuel electrode. Therefore, to achieve sufficiently enhanced electrode activity and reduce the op-

erating temperature, modifying the active sites of the electrode surface is considered the most efficient method.

Fig. 6a depicts the schematic operating principle under the SOFC mode, which demonstrates the generation of electrical power by the oxidation of CO to CO<sub>2</sub>. Furthermore, Fig. 6b shows the schematic operating principle under the SOEC mode, which highlights the storage of electrical power in CO from CO<sub>2</sub> reduction. Evidently, both CO oxidation reactions and CO<sub>2</sub> reduction reactions occur at the fuel electrode. To clarify the significance of our phase-transformed fuel electrode, a single cell supported on the YSZ electrolyte was fabricated (SEM images in Fig. S2a). In Fig. 3b, microsized SFMCo particles before reduction are interconnected with one another to form a continuous pathway for electron-ion transportation while showing a rounded and smooth surface. After the phase-transformation into CoFe-SFM (confirmed by the XRD pattern in Fig. 2b) in hydrogen, the electrode surface becomes rough (Fig. S2c). Well dispersed CoFe alloy nanoparticles appear over the micron-sized SFM grains (Fig. S2d), which successfully indicates the catalytic capability of our desired fuel electrode. In this case, the single cell is operated using a 2:1 CO-CO<sub>2</sub> mixture fed to the fuel electrode and LSM-SDC oxygen electrode in

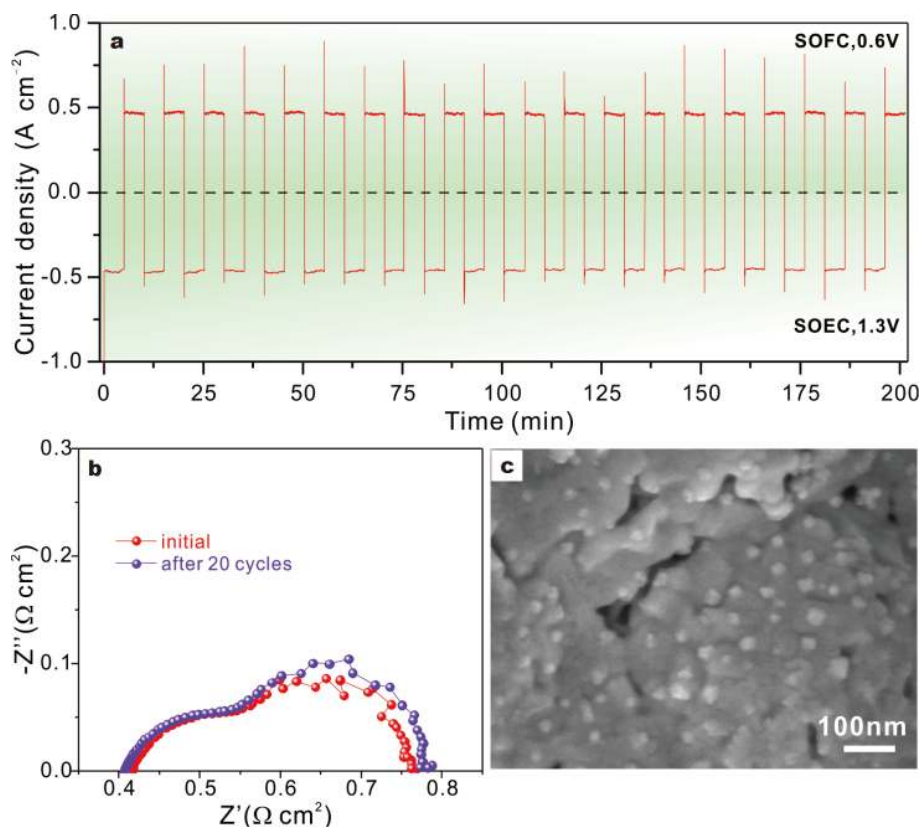


**Figure 6** (a, b) Schematic of the (a) SOFC mode for CO oxidation and (b) SOEC mode for CO<sub>2</sub> reduction. (c, d) Comparison of the electrochemical performance of the CoFe-SFM cell and SFMCo cell at 800°C under the (c) SOFC mode and (d) SOEC mode.

ambient air. Fig. 6c compares the electrochemical performances of the CoFe-SFM- and SFMCo-based cells under the SOFC mode at 800°C. The positive current density represents the generated electricity when CO fuels are oxidized into CO<sub>2</sub>. Before the reduction, the cell with the SFMCo fuel electrode shows a maximum power density (MPD) of approximately  $\sim 100 \text{ mW cm}^{-2}$ . After full annealing in hydrogen and the feeding gas has been switched back to 2:1 CO-CO<sub>2</sub>, the cell with the SFMCo fuel electrode shows an increased MPD of approximately  $259 \text{ mW cm}^{-2}$  by a factor of  $\sim 1.5$ . The cell also displays appreciable MPDs of 194 and  $136 \text{ mW cm}^{-2}$  at 750 and 700°C, respectively (Fig. S3). We calculated the corresponding CO conversion rate at 800°C, assuming a 100% current efficiency because of the unity ionic transport number in YSZ; it increased from 1.644 to  $3.079 \text{ mL min}^{-1} \text{ cm}^{-2}$ . Fig. 6d compares the electrochemical performance under the SOEC mode at 800°C. The negative current density suggests the electricity energy storage as CO<sub>2</sub> is decomposed into CO and O<sub>2</sub>. The cell with the CoFe-SFM fuel electrode achieves a current density of  $-0.453 \text{ A cm}^{-2}$  at 1.3 V, which is much higher

than that of the cell with the SFMCo fuel electrode ( $-0.291 \text{ A cm}^{-2}$ ) under identical operating voltage condition. The corresponding CO<sub>2</sub> conversion rate increases by 55.67% from 2.027 to  $3.155 \text{ mL min}^{-1} \text{ cm}^{-2}$ . The cell also outputs good current densities of  $-0.350$  and  $-0.226 \text{ A cm}^{-2}$  at 1.3 V at 750 and 700°C, respectively (Fig. S3). Thus, this considerable enhancement of CO oxidation and CO<sub>2</sub> reduction kinetics is entirely attributed to a synergy effect between highly active CoFe alloy and SFM with abundant defects [57]. Since the electrolyte and oxygen electrode do not change in either cell, the considerably improved performance suggests the superiority of the CoFe-SFM fuel electrode.

To demonstrate the reversible operation between SOFC and SOEC modes, the single cell was examined at 800°C using two switching voltages: a voltage of 1.3 V higher than OCV for the CO<sub>2</sub> reduction and a lower voltage of 0.6 V for the CO oxidation. As shown in Fig. 7a, first, the cell was operated under a constant voltage of 1.3 V (SOEC mode) for 5 min to generate CO. Subsequently, the cell was instantly switched to the SOFC mode using a constant voltage of 0.6 V for the same duration. The



**Figure 7** (a) Reversible 20-cycle test performance at 0.6 V (SOFC mode) and 1.3 V (SOEC mode); (b) EIS plots before and after the reversible cycle test; (c) high-resolution SEM image of the CoFe-SFM fuel electrode after the test.

stable current densities in each SOEC-SOFC cycle suggest that the reversible operation did not cause a significant negative effect on the performance of our cell with the CoFe-SFM fuel electrode. Fig. 7b compares the Nyquist plots under OCV conditions before and after the 20-cycle test, which shows no apparent change. Furthermore, the cell was broken into small pieces for the post-SEM characterization. In Fig. 7c, exsolved CoFe nanoparticles remain uniformly anchored on the SFM substrate without much agglomeration. Carbon deposition was not observed either. These two points prove that CoFe-SFM is an excellent fuel electrode with good durability, good carbon resistance, and successful CO/CO<sub>2</sub> conversion in RSOC. Thus, it has enormous potential for utilizing and storing renewable energy and yielding valuable chemicals.

## CONCLUSIONS

We have demonstrated that the phase-transformed CoFe-SFM composite material can be developed as an efficient fuel electrode for RSOC. Both EIS and DRT studies suggest that the CO/CO<sub>2</sub> conversion performance was significantly improved by accelerating the bulk oxygen diffusion and surface reaction kinetics on the CoFe-SFM fuel electrode, which improved the CO<sub>2</sub> reduction rate by 55.67%@1.3 V and CO oxidation rate by 150% at 800°C compared with the control sample. Moreover, RSOCs with the CoFe-SFM electrode demonstrated excellent cyclability and durability in 20 cycle operations. Therefore, this study may provide future guidance for designing fuel electrodes and utilizing RSOC for efficient CO<sub>2</sub> conversion and utilization. A long reversible operation is required and currently performed in the lab, and the result will be reported soon.

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**Author contributions** Fan L and Li Y conceived the idea, designed the experiments, analyzed the data and wrote the manuscript. Singh M and Zhuang Z performed the material microstructure characterization. Jing Y and Maliutina K participated in device optimization and data analysis. Li Y drafted the manuscript. He C and Fan L contributed to the final version of the manuscript. All authors contributed to the general discussion and reviewed the manuscript.

**Conflict of interest** The authors declare that they have no conflict of interest.

**Supplementary information** The XPS O 1s spectra, SEM images of typical cells, the temperature dependence of RSOC electrochemical performance, EIS fitting and DRT deconvolution results are available in the online version of the paper.



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## 相变燃料电极实现固体氧化物电池高效可逆CO/CO<sub>2</sub>转化

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**摘要** 固体氧化物电池可实现CO/CO<sub>2</sub>的可逆转化, 在电能和化学能相互转化过程中显示出巨大潜力. 然而, 其商业化进展一直受到燃料极抗积碳性能差的限制. 本工作中, 我们发展了一种CoFe合金纳米颗粒和Ruddlesden-Popper层状结构Sr<sub>3</sub>Fe<sub>1.25</sub>Mo<sub>0.75</sub>O<sub>7-δ</sub>复合新型燃料电极(CoFe-SFM), 其可以通过钙钛矿Sr<sub>2</sub>Fe<sub>7/6</sub>Mo<sub>0.5</sub>Co<sub>1/3</sub>O<sub>6-δ</sub>在还原气氛中退火发生相变得到. 电化学阻抗谱和弛豫时间分步法分析可知CoFe-SFM电极通过改善体相氧化学扩散能力和表面氧交换过程来增强CO氧化和CO<sub>2</sub>还原动力学. 在固体氧化物燃料电池模式下, 800°C的最大功率达到259 mW cm<sup>-2</sup>; 在固体氧化物电解池模式下, 1.3 V工作电压下单电池的电解电流密度为-0.453 A cm<sup>-2</sup>, 都远超对比电极材料. 在20次SOFC-SOEC循环操作条件下, CoFe-SFM燃料极依然保持稳定的微结构和抗积碳性能, 电池性能保持良好. 该工作可为CO<sub>2</sub>转化、抗积碳电极材料设计和提升电极表界面反应动力学提供一定的指导作用.